

Stokes' law and intrinsic viscosity coefficient in complex liquids

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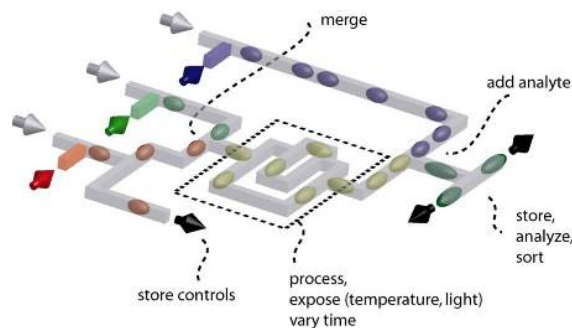
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Motivation

December 2015



Piotr Garstecki



+ ~20 group members

Diffusion in biological
systems and complex
liquids

.....


Robert Hołyst



+ ~20 group members

Motivation – scaling with radius of particle

Observation in experiments with diffusion on complex liquids

$$D \neq \frac{k_B T}{6\pi\eta a}$$




In complex liquids scaling with a may be dramatically different!

Different scaling also observed at many systems, e.g.

Thomas Gisler and David A Weitz. PRL, 82(7):1606, 1999

It happens when size of the particles is comparable to length characterizing complex liquid

Roseanna N Zia and John F Brady. Theoretical microrheology 113-157. Springer, 2015

Goal

What is the scaling of **diffusion coefficient** with **size** of the particle in complex liquid?

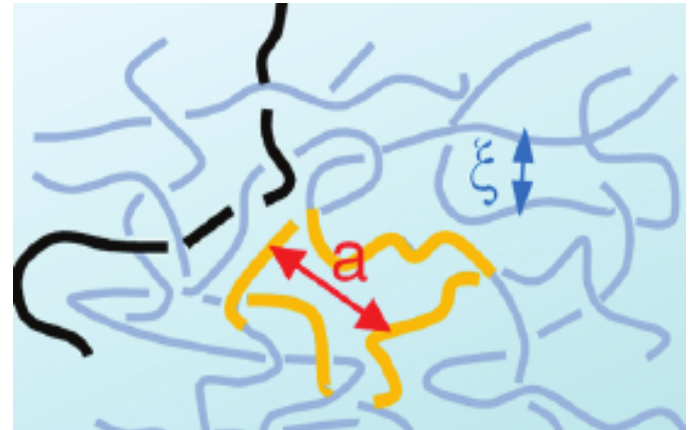
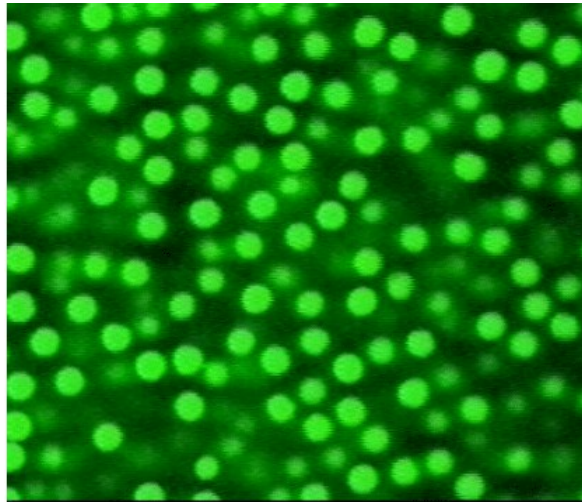
What is the relation between **diffusion** and **viscosity** of complex liquid?



Complex liquids

Liquids with polyatomic structures

Examples: colloidal suspensions, polymer liquids, cell cytoplasm, ...



Frequency and wave-vector-dependent viscosity

Difference between simple and complex liquids:

simple liquid

$$\eta = \text{const}$$

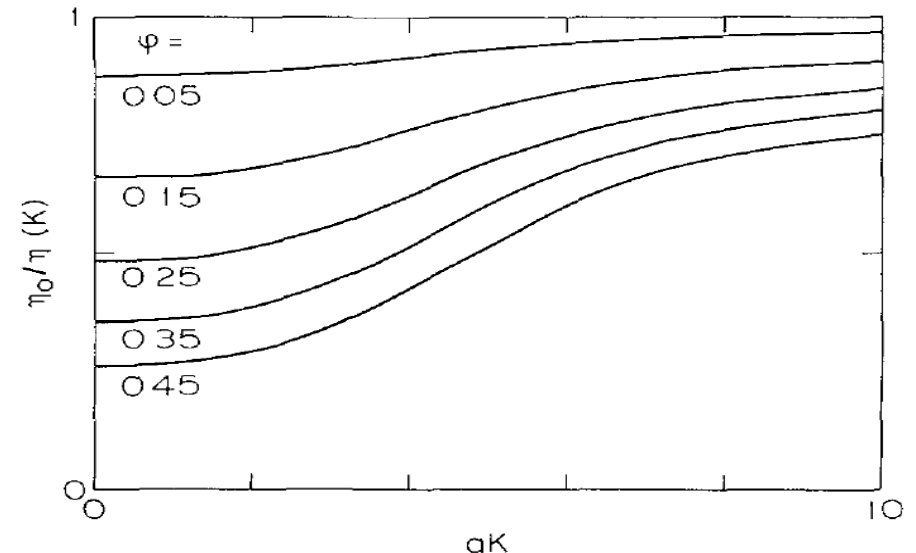
complex liquid

$$\eta(\omega, k)$$

Smoluchowski dynamics with
hydrodynamic interactions and direct
interactions between particles
suspended in fluid

+

linear response theory



Szymczak, P. & Cichocki, B. Journal of
Statistical Mechanics: Theory and Experiment,
2008, P0102

Beenakker, C. W. J. Physica A: Statistical and
Theoretical Physics, Elsevier, 1984, 128, 48-8

Consequences of linear response theory

Linear response:

$$V(\omega) = \zeta(\omega)F(\omega)$$

Fluctuation-dissipation theorem:

$$D(\omega) = \frac{k_B T}{\zeta(\omega)}$$

Assumption valid for **big particles** (bigger than all characteristic length scales of complex fluid):

Stokes' law

$$\zeta(\omega) = 6\pi\eta(\omega)a$$

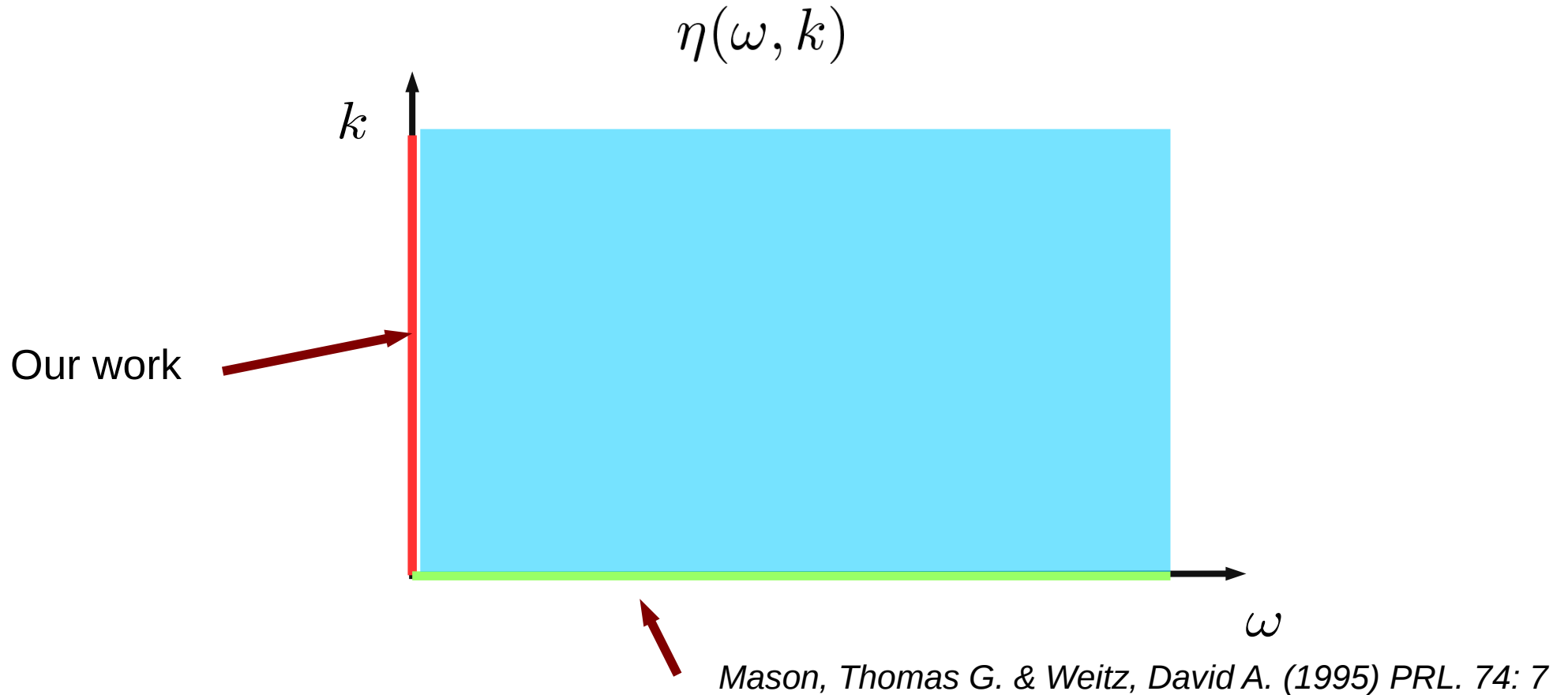
Active microrheology

Passive microrheology

Invalid for small particles

The diagram illustrates the consequences of linear response theory. It shows a cycle of relationships: Linear response theory leads to the equation $V(\omega) = \zeta(\omega)F(\omega)$, which is linked to the Fluctuation-dissipation theorem $D(\omega) = \frac{k_B T}{\zeta(\omega)}$. Both are based on the assumption that the theory is valid for big particles. This leads to Stokes' law $\zeta(\omega) = 6\pi\eta(\omega)a$, which is used in both active and passive microrheology. A red arrow points from the text 'Invalid for small particles' to the Stokes' law equation, indicating its limitation.

Current stage of microrheology in complex liquids

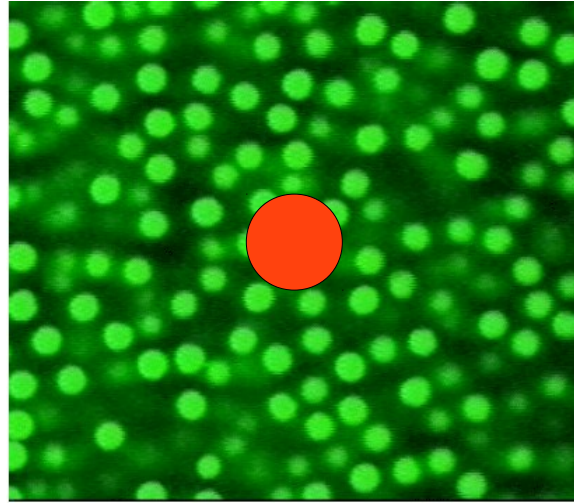


Current stage of knowledge – in the literature there is no generalization of the Stokes' law for wave-vector-dependent viscosity. Therefore there is no theoretical foundation for microrheology with small particles.

There is also no generalization for arbitrary frequency and wave-vector

Goals of our work

Spherical particle immersed in complex liquid



$$\eta(k)$$

Mean-field

1) Drag force on spherical particle moving in complex liquid:

$$\mathbf{F} = \zeta(a) \mathbf{U}$$

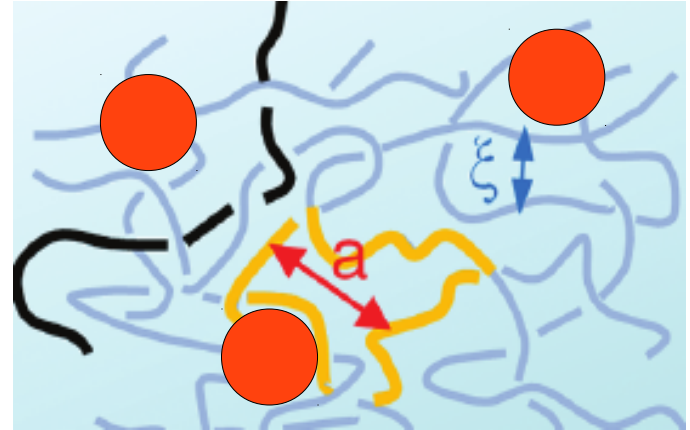
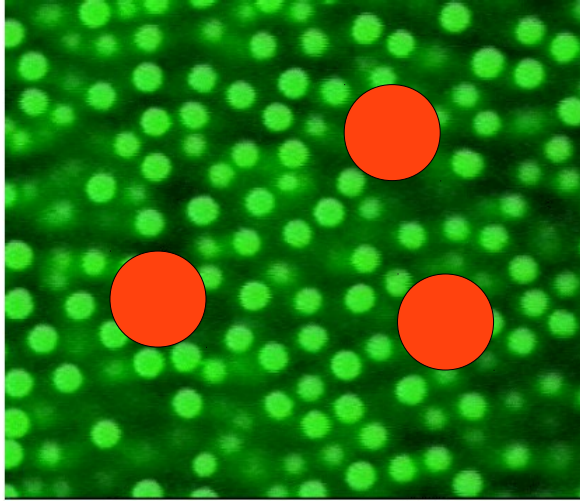
Friction coefficient

Stokes law in simple liquids:

$$\zeta(a) = 6\pi\eta a$$

Goals of our work

Add particles to complex liquids



2) Increase of viscosity

$$\eta_{\text{eff}} = \eta(0) (1 + E(a) \phi)$$

intrinsic viscosity coefficient



intrinsic viscosity coefficient
(simple liquids):

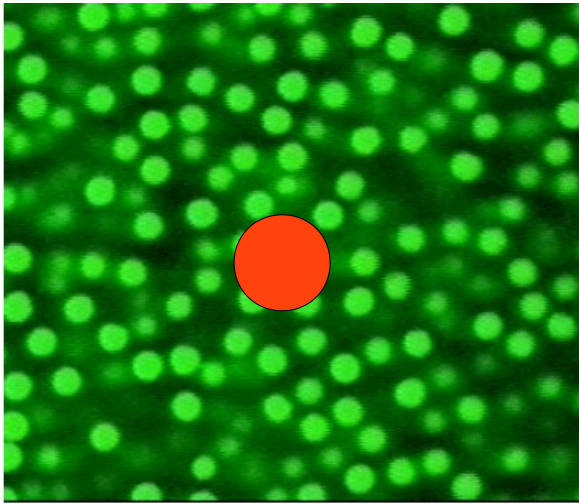
$$E(a) = 5/2$$

Stokes law in complex liquids – formulation of the problem

Stokes equations in complex liquids viscosity depends on scale:

$$i\mathbf{k}p + k^2\eta(k)\hat{\mathbf{v}}(\mathbf{k}) = 0,$$

$$\mathbf{k} \cdot \hat{\mathbf{v}}(\mathbf{k}) = 0.$$



Boundary conditions:

$$\mathbf{v}(\mathbf{r}) = \mathbf{U} \quad \text{for } |\mathbf{r}| = a$$

$$\mathbf{v}(\mathbf{r}) \rightarrow 0 \quad \text{for } r \rightarrow \infty$$

What is the friction coefficient $\zeta(a)$?

$$\mathbf{F} = \zeta(a) \mathbf{U}$$

Stokes law in complex liquids – idea of derivation

Difference between simple and complex liquids:

simple liquid

$$\eta \Delta$$



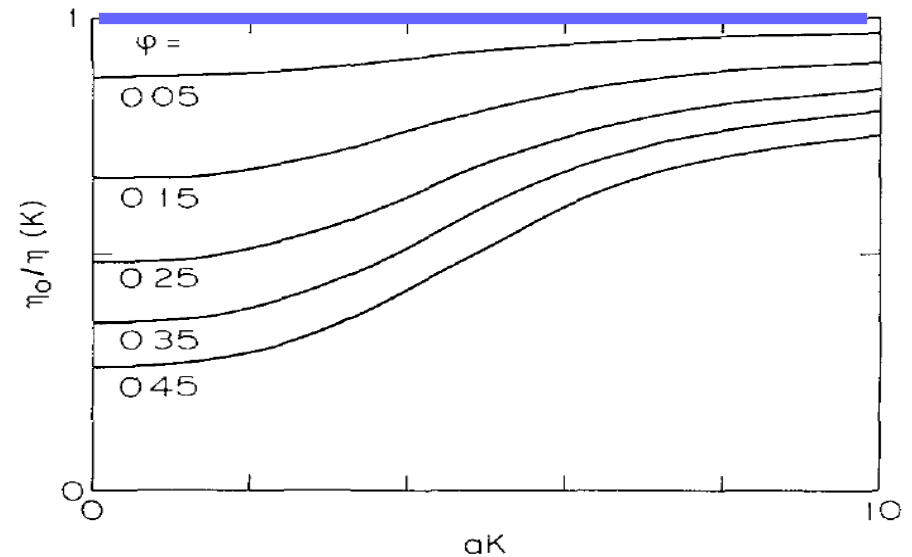
complex liquid

$$\eta(\Delta) \Delta$$

$$\eta = \text{const}$$



$$\eta(k)$$



Linearity and spherical symmetry (isotropic fluid, spherical particle) strongly simplifies derivation in simple fluids, $\eta = \text{const}$

Idea: Derive the Stokes law in simple liquids in **Fourier space** and with use of **spherical symmetry**, and **generalize** it to the case of scale dependent viscosity

Stokes law in simple liquids – idea of derivation that uses symmetry and Fourier space

Ansatz for velocity field:

$$\hat{\mathbf{v}}(\mathbf{k}) = \hat{\mathbf{v}}_0(\mathbf{k}) + c\hat{\mathbf{v}}_1(\mathbf{k})$$

$$\begin{aligned} i\mathbf{k}p_0 + k^2\eta\hat{\mathbf{v}}_0(\mathbf{k}) &= \mathbf{F}, \\ \mathbf{k} \cdot \hat{\mathbf{v}}_0(\mathbf{k}) &= 0. \end{aligned}$$

$$\hat{\mathbf{v}}_0(\mathbf{k}) = \frac{1}{\eta k^2} (1 - \hat{\mathbf{k}}\hat{\mathbf{k}}) \mathbf{F}$$

$$\Delta \mathbf{v}_1(\mathbf{r}) = 0$$

$$\mathbf{v}_1(\mathbf{r}) = \frac{1}{4\pi r^3} (1 - 3\hat{\mathbf{r}}\hat{\mathbf{r}}) \mathbf{F}$$

Boundary conditions on the surface of particle, applied to the above ansatz lead to c, \mathbf{F}

$$\mathbf{v}(a\hat{\mathbf{r}}) = \mathbf{U}$$

$$\mathbf{F} = 6\pi\eta a\mathbf{U}$$

Stokes law – generalization to the case of complex liquids

Ansatz for velocity field:

$$\hat{\mathbf{v}}(\mathbf{k}) = \hat{\mathbf{v}}_0(\mathbf{k}) + c\hat{\mathbf{v}}_1(\mathbf{k})$$

$$\begin{aligned} i\mathbf{k}p_0 + k^2\eta(k)\hat{\mathbf{v}}_0(\mathbf{k}) &= \mathbf{F}, \\ \mathbf{k} \cdot \hat{\mathbf{v}}_0(\mathbf{k}) &= 0. \end{aligned}$$

$$\hat{\mathbf{v}}_0(\mathbf{k}) = \frac{1}{\eta(k)k^2} (\mathbf{1} - \hat{\mathbf{k}}\hat{\mathbf{k}}) \mathbf{F}$$

$$\eta(\Delta) \Delta \mathbf{v}_1(\mathbf{r}) = 0$$

$$\mathbf{v}_1(\mathbf{r}) = \frac{1}{4\pi r^3} (\mathbf{1} - 3\hat{\mathbf{r}}\hat{\mathbf{r}}) \mathbf{F}$$

*Boundary conditions on the surface of particle, $\mathbf{v}(a\hat{\mathbf{r}}) = \mathbf{U}$
applied to the above ansatz lead to*

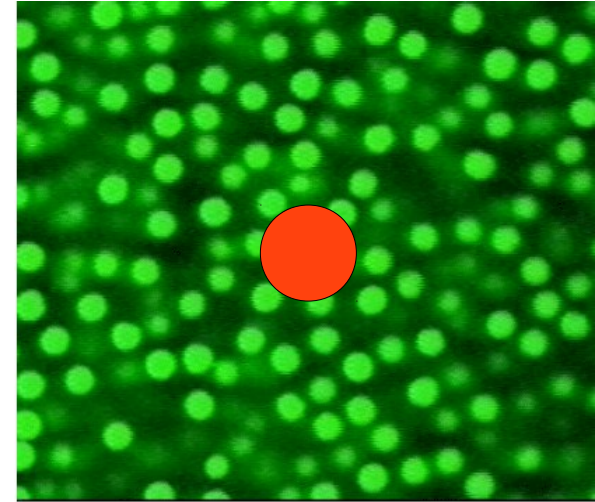
$$\mathbf{U} = \frac{1}{(2\pi)^3} \int d^3k e^{ia\hat{\mathbf{r}}\mathbf{k}} \frac{1}{\eta(k)k^2} (\mathbf{1} - \hat{\mathbf{k}}\hat{\mathbf{k}}) \mathbf{F} + c \frac{1}{4\pi r^3} (\mathbf{1} - 3\hat{\mathbf{r}}\hat{\mathbf{r}}) \mathbf{F}$$

which yields...

Stokes' law in complex liquids

What is the friction coefficient?

$$\mathbf{F} = \zeta(a) \mathbf{U}$$



$$\zeta(a) = \frac{3\pi^2}{\int_0^\infty dk \frac{j_0(ka)}{\eta(k)}}$$

$$j_0(x) = \sin(x) / x$$

Application of the Stokes law in complex liquids

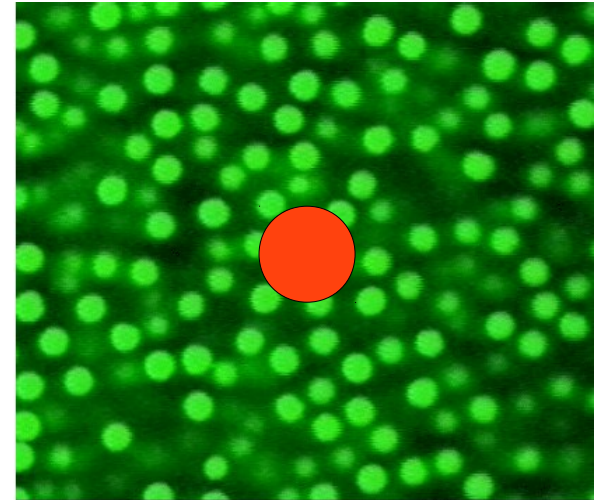
- from friction coefficient to scale dependent viscosity

Stokes law: from scale dependent viscosity to friction coefficient

$$\zeta(a) = 3\pi^2 / \left(\int_0^\infty dk j_0(ka) / \eta(k) \right)$$



Fourier transform



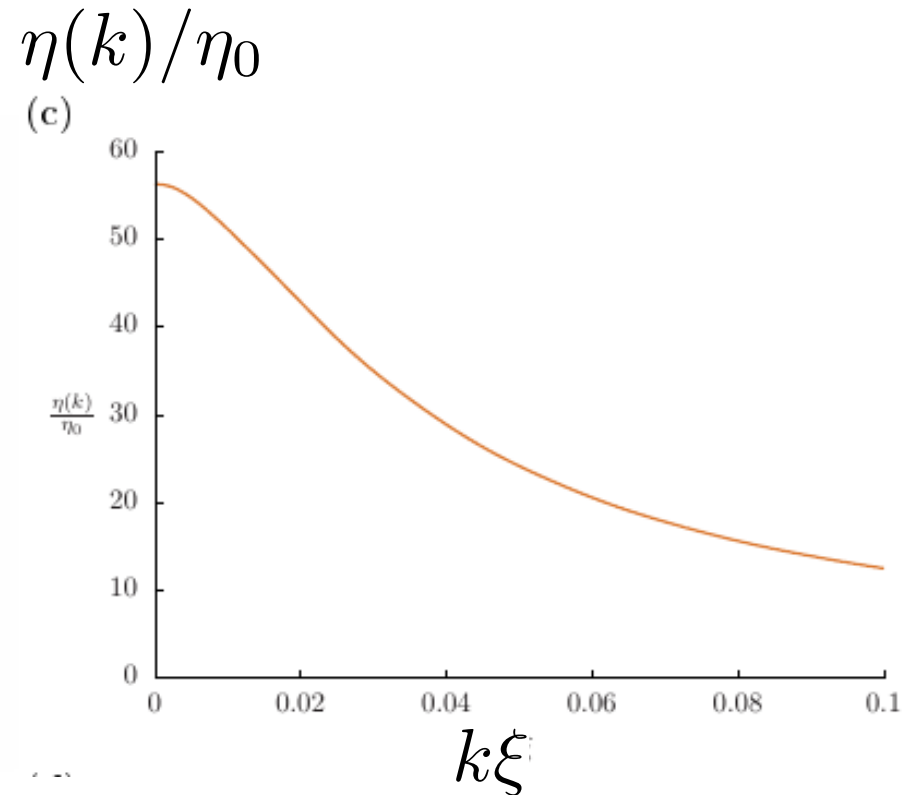
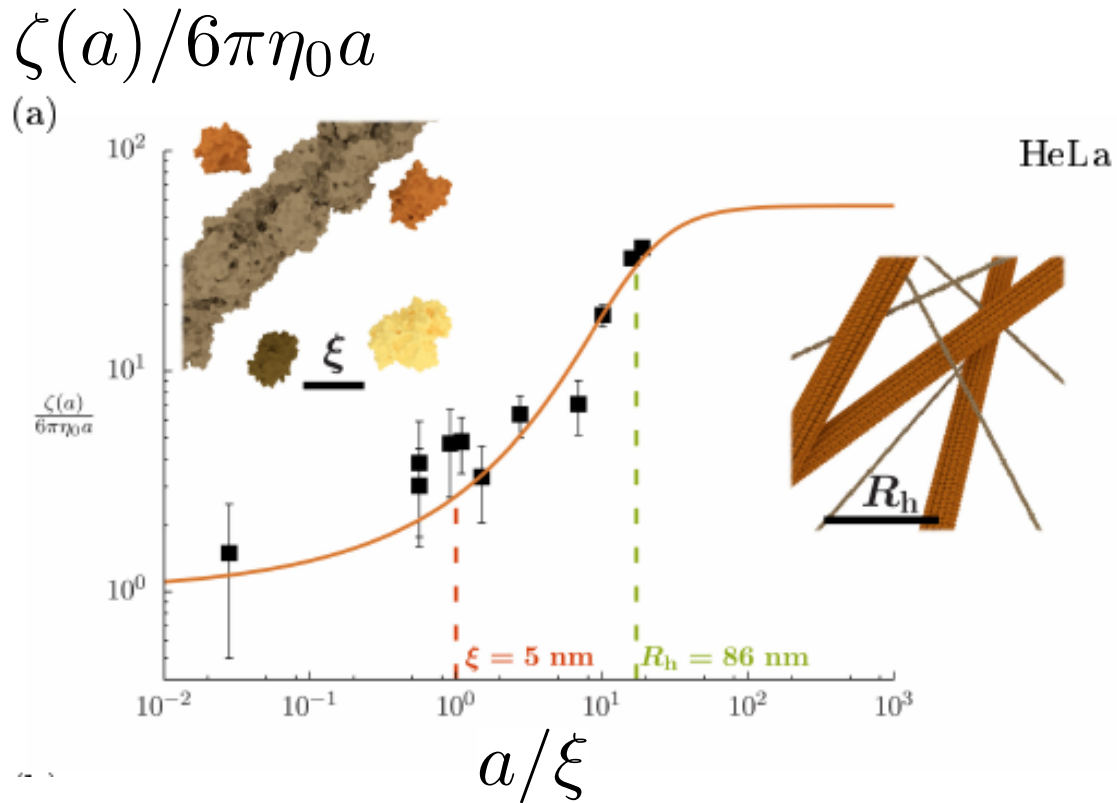
friction coefficient from scale dependent viscosity:

$$\eta(k) = \frac{1}{6\pi k^2} \left[\int_0^\infty da a^2 \frac{j_0(ak)}{\zeta(a)} \right]^{-1}$$

Friction from passive or active microrheological experiments

Application of the Stokes' law in complex liquids

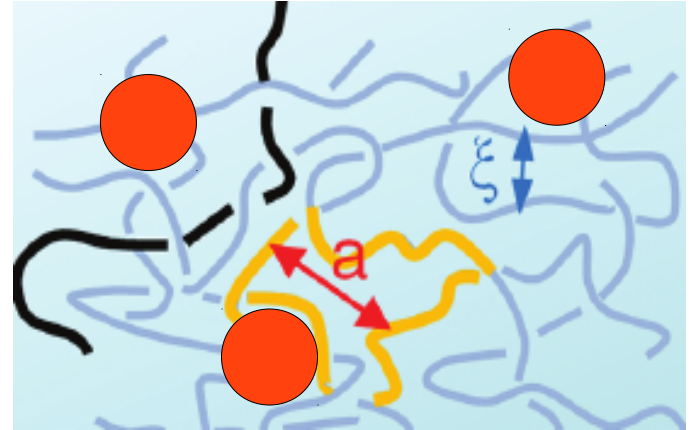
- from friction coefficient to scale dependent viscosity



Friction coefficient of different particles inside HeLa cell cytoplasm

Intrinsic viscosity coefficient $E(a)$ in complex liquids

$$\eta_{\text{eff}} = \eta(0) (1 + E(a) \phi)$$



$$E(a) = -\frac{5}{2} \frac{1}{\eta(0)} \left[\frac{10}{3\pi} a^2 \frac{d}{da} \int_0^\infty dk \frac{j_0(ak)}{\eta(k)} + \frac{4}{\pi} a \int_0^\infty dk \frac{j_2(ak)}{\eta(k)} + \frac{4a^2}{3\pi} \frac{d}{da} \int_0^\infty dk \frac{j_2(ak)}{\eta(k)} \right]^{-1}$$

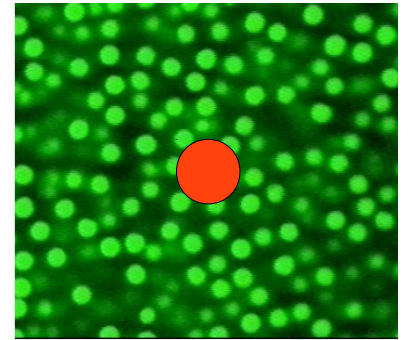
$$j_0(x) = \sin(x)/x$$

$$j_2(x) = -\sin(x)/x - 3\cos x/x^2 + 3\sin(x)/x^3$$

Intrinsic viscosity coefficient and Stokes' friction coefficient

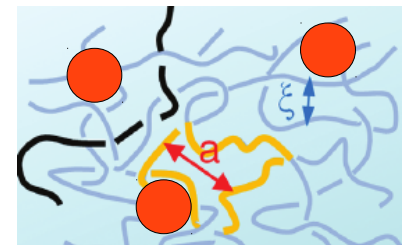
Stokes law in complex liquids:

$$\zeta(a) = 3\pi^2 / \left(\int_0^\infty dk j_0(ka) / \eta(k) \right)$$



Einstein viscosity coefficient in complex liquids:

$$E(a) = -\frac{5}{2} \frac{1}{\eta(0)} \left[\frac{10}{3\pi} a^2 \frac{d}{da} \int_0^\infty dk \frac{j_0(ak)}{\eta(k)} + \frac{4}{\pi} a \int_0^\infty dk \frac{j_2(ak)}{\eta(k)} + \frac{4a^2}{3\pi} \frac{d}{da} \int_0^\infty dk \frac{j_2(ak)}{\eta(k)} \right]^{-1}$$



Universal relation between friction and intrinsic viscosity coefficient

$$E(a) = \frac{5}{12\pi\eta(0)a^2} \frac{\zeta(a)^2}{\frac{d\zeta(a)}{da}}$$

Summary

- Stokes law in complex liquids,
- Intrinsic viscosity coefficient,
- Universal relation between intrinsic viscosity coefficient and friction coefficient

... when viscosity is scale-dependent (depends on wave-vector)
and does not depend on frequency